

Heat Flow Across the San Andreas Fault



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11/02/2015

Calculating Shear Stress on the San Andreas Fault

$$\tau(z) = f \sigma_n$$

Where $\sigma_n = \rho_c g z$

$\tau(z)$ shear stress on a locked fault

σ_n normal force

f coefficient of static friction

ρ_c crustal density

g acceleration due to gravity

z depth of seismogenic zone

Calculating Shear Stress on the San Andreas Fault

San Andreas Fault Assumptions

$$f = 0.6$$

$$\rho_c = 2600 \text{ kg m}^{-3}$$

$$g = 9.8 \text{ m s}^{-2}$$

$$z = 12 \text{ km}$$

$$\tau(z) = 183 \text{ MPa}$$

PROBLEM – Average stress drop on a fault during an actual earthquake $\leq 10 \text{ MPa}$

Calculating Shear Stress on the San Andreas Fault

Considerations

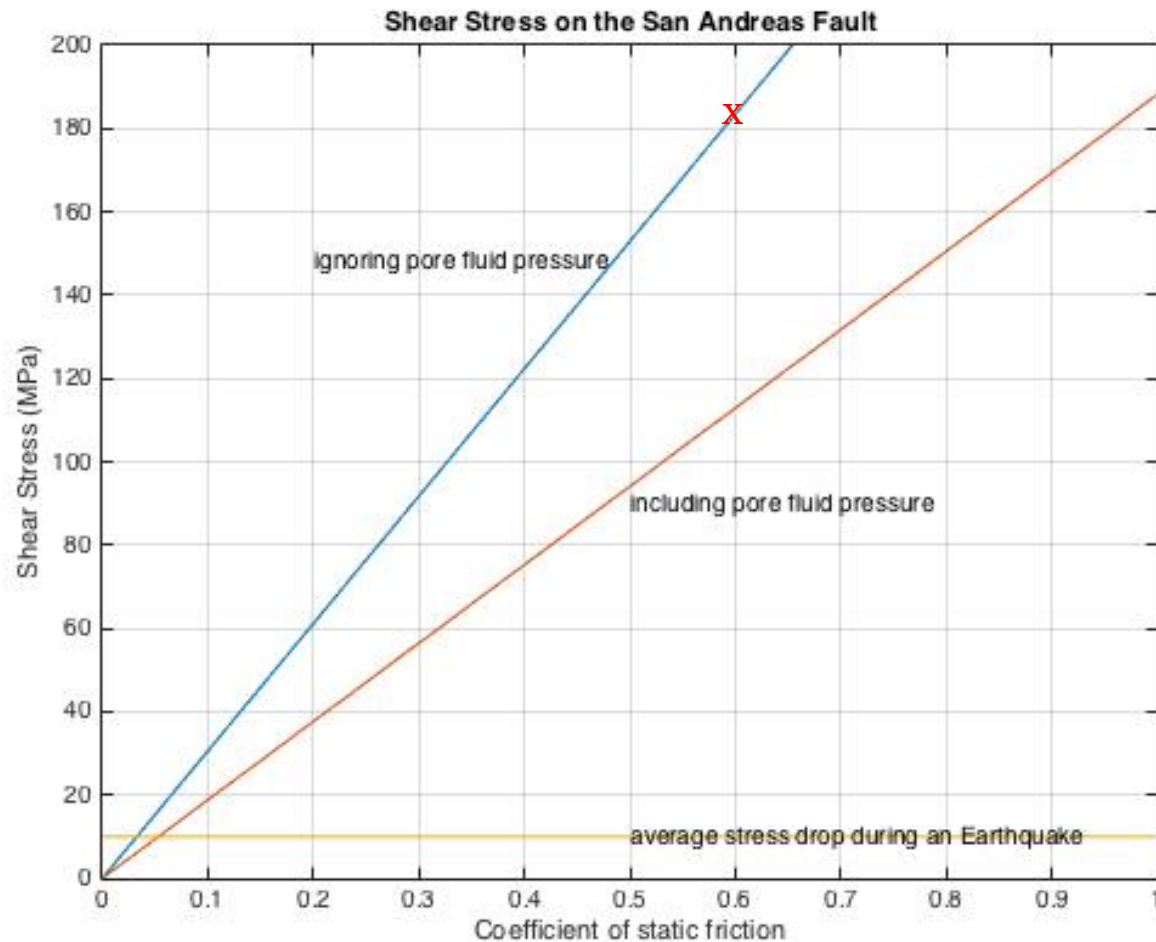
Coefficients of Static Friction

f varies with depth

Pore fluid pressure

$$\sigma = \sigma_n - \sigma_{\text{pore fluid pressure}} \text{ so } \tau(z) = f(\rho_c - \rho_w)gz$$

Calculating Shear Stress



Derivation of a Line Source of Heat to get Heat Flow Anomaly

- We want to model the heat flow off of the San Andreas Fault as a line source of heat that dissipates as one moves away from the fault
- We need to get an equation that can be used to calculate the heat flow anomaly for different coefficients of static friction given an equation for a temperature anomaly
- Method
 - Start with an equation for a temperature anomaly and take a Fourier Transform
 - Take the inverse Fourier Transform in two dimensions to receive an easier temperature function to work with
 - Use the relationship between temperature and heat flow to get our heat flow anomaly equation

Derivation of Heat Flow from a Line Source

Given:

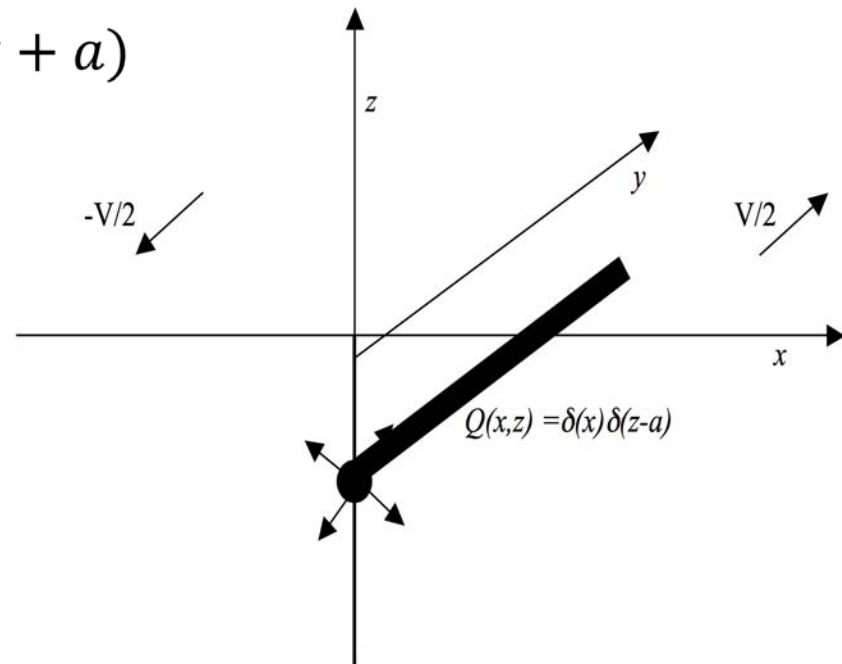
$$\nabla^2 T = \frac{1}{k} Q(x, z) = \frac{1}{k} \delta(x) \delta(z + a)$$

$$\nabla^2 T = \frac{d^2 T}{dx^2} + \frac{d^2 T}{dz^2}$$

$$T(x, 0) = 0$$

$$\lim_{|z| \rightarrow \infty} T(x, z) = 0$$

$$\lim_{|x| \rightarrow \infty} T(x, z) = 0$$



T = Temperature Anomaly
 k = Thermal Conductivity = 3.3 W/mK
 Q = Heat Generation

Step 1: Take Fourier Transform with Respect to x and z

$$\frac{d^2 T}{dx^2} + \frac{d^2 T}{dz^2} = \frac{1}{k} \delta(x) \delta(z + a)$$

- Use the derivative property of Fourier Transforms: $\mathfrak{F}\left[\frac{\partial f}{\partial x}\right] = i2\pi k F(k)$

$$[(i2\pi k_x)^2 + (i2\pi k_z)^2][T(k_x, k_z)] = \mathfrak{F}t(\delta(x)\delta(z + a))$$

- Use property for the transform of a delta function: $F[\delta(x - x_o)] = e^{-i2\pi f(x_o)}$

$$4\pi^2(k_x^2 + k_z^2)T(k_x, k_z) = \int_{-\infty}^{\infty} \delta(x) e^{i2\pi k_x x} dk_x \int_{-\infty}^{\infty} \delta(z + a) e^{i2\pi k_z(z+a)} dk_z \quad F[\delta(x)] = 1$$

- Which when simplified equals:
 $-4\pi^2(k_x^2 + k_z^2)T(k_x, k_z) = 1 * e^{-i2\pi k_z a}$

$$T(k_x, k_z) = \frac{e^{-i2\pi k_z a}}{-4\pi^2(k_x^2 + k_z^2)}$$

- Rearranging for T yields:

Step 2: Take the Inverse Fourier Transform with Respect to k_z

$$T(k_x, k_z) = \frac{e^{-i2\pi k_z a}}{-4\pi^2(k_x^2 + k_z^2)}$$

Note that: $(k_x^2 + k_z^2) = (k_z + ik_x)(k_z - ik_x)$

$$T(k_x, z) = \frac{-1}{4\pi^2} \int_{-\infty}^{\infty} \frac{e^{i2\pi k_z(z+a)}}{(k_z + ik_x)(k_z - ik_x)} dk_z$$

Cauchy Residue Theorem

- If a function is analytic, integrating around complex poles on a closed loop will equal zero

$$\oint f(z)dz = 0$$

- If we have complex poles in the denominator of the function, the Cauchy Residue theorem states

$$\oint \frac{f(z)}{z - z_0} = i2\pi f(z_0)$$

Step 2: Take the Inverse Fourier Transform with Respect to k_z

$$T(k_x, z) = \frac{-1}{4\pi^2} \int_{-\infty}^{\infty} \frac{e^{i2\pi k_z(z+a)}}{(k_z + ik_x)(k_z - ik_x)} dk_z$$

$$\oint \frac{f(z)}{z - z_0} = i2\pi f(z_0)$$

If $k_z = ik_x$, considering $k_x > 0$ and $z > -a$

$$T(k_x, z) = (i2\pi) \frac{-1}{4\pi^2} \frac{e^{i2\pi k_x(z+a)}}{(ik_x + ik_x)}$$

$$T(k_x, z) = \frac{-1}{4\pi} \frac{e^{-2\pi k_x(z+a)}}{k_x}$$

If $k_z = -ik_x$, considering $k_x < 0$ and $z > -a$

$$T(k_x, z) = (i2\pi) \frac{-1}{4\pi^2} \frac{e^{-i2\pi k_x(z+a)}}{(-ik_x - ik_x)}$$

$$T(k_x, z) = \frac{1}{4\pi} \frac{e^{2\pi k_x(z+a)}}{k_x}$$

Combine the last two equations using the absolute value of k_x

$$T(k_x, z) = \frac{-1}{4\pi} \frac{e^{-2\pi |k_x|(z+a)}}{|k_x|}$$

Step 3: Take the Inverse Fourier Transform with Respect to k_x

$$T(x, z) = \frac{-1}{4\pi} \int_{-\infty}^{\infty} \frac{e^{-2\pi|k_x|(z+a)}}{|k_x|} e^{i2\pi k_x x} dk_x$$

- Using the derivative property of Fourier Transforms

$$\frac{\partial T(x, z)}{\partial z} = i2\pi k_z \frac{-1}{4\pi} \int_{-\infty}^{\infty} \frac{e^{-2\pi|k_x|(z+a)}}{|k_x|} e^{i2\pi k_x x} dk_x$$

$$\frac{\partial T(x, z)}{\partial z} = \frac{1}{2} \int_{-\infty}^{\infty} e^{-2\pi|k_x|(z+a)} e^{i2\pi k_x x} dk_x$$

$$\frac{\partial T(x, z)}{\partial z} = \frac{-(z+a)}{4\pi[x^2 + (z+a)^2]}$$

Step 3: Take the Inverse Fourier Transform with Respect to k_x

- Integrating with respect to z

$$T(x, z) = \frac{-1}{4\pi} \ln([x^2 + (z + a)^2]^{\frac{1}{2}})$$

- Because this does not satisfy our boundary conditions, we must add a heat sink at $z = a$, giving us our final equation that satisfies all boundary conditions.

$$T(x, z) = \frac{-1}{4\pi} [\ln([x^2 + (z + a)^2]^{\frac{1}{2}}) - \ln([x^2 + (z - a)^2]^{\frac{1}{2}})]$$

$$T(x, z) = \frac{-1}{4\pi} \ln \left(\frac{(x^2 + (z + a)^2)}{(x^2 + (z - a)^2)} \right)^{\frac{1}{2}}$$

Step 4, take our temperature anomaly and find heat flow

- We have temperature in terms of z and x , now we need to find the heat flow q by integrating with respect to a

$$q(x, z, a) = -k \frac{\partial T}{\partial z} = \frac{1}{4\pi} \left(\frac{z + a}{x^2 + a^2} - \frac{z - a}{x^2 + a^2} \right)$$

- To satisfy our boundary conditions, we need to set z equal to zero, thus we get

$$q(x, a) = \frac{1}{4\pi} \frac{2a}{x^2 + a^2}$$

Aside: Green's Function

- Now we must use a Green's function to evaluate heat flow over our heat source by using the following relation:

$$q(x) = \int q(x, a) f(a) da$$

- For us, $f(a)$ is the heat generated due to frictional heating, which we also have:

$$f(a) = v \cdot \tau = v \mu \rho_c g a$$

- Where v is the mean velocity of the plate: San Andreas Fault: 35mm/year

Step 4, take our temperature anomaly and find heat flow

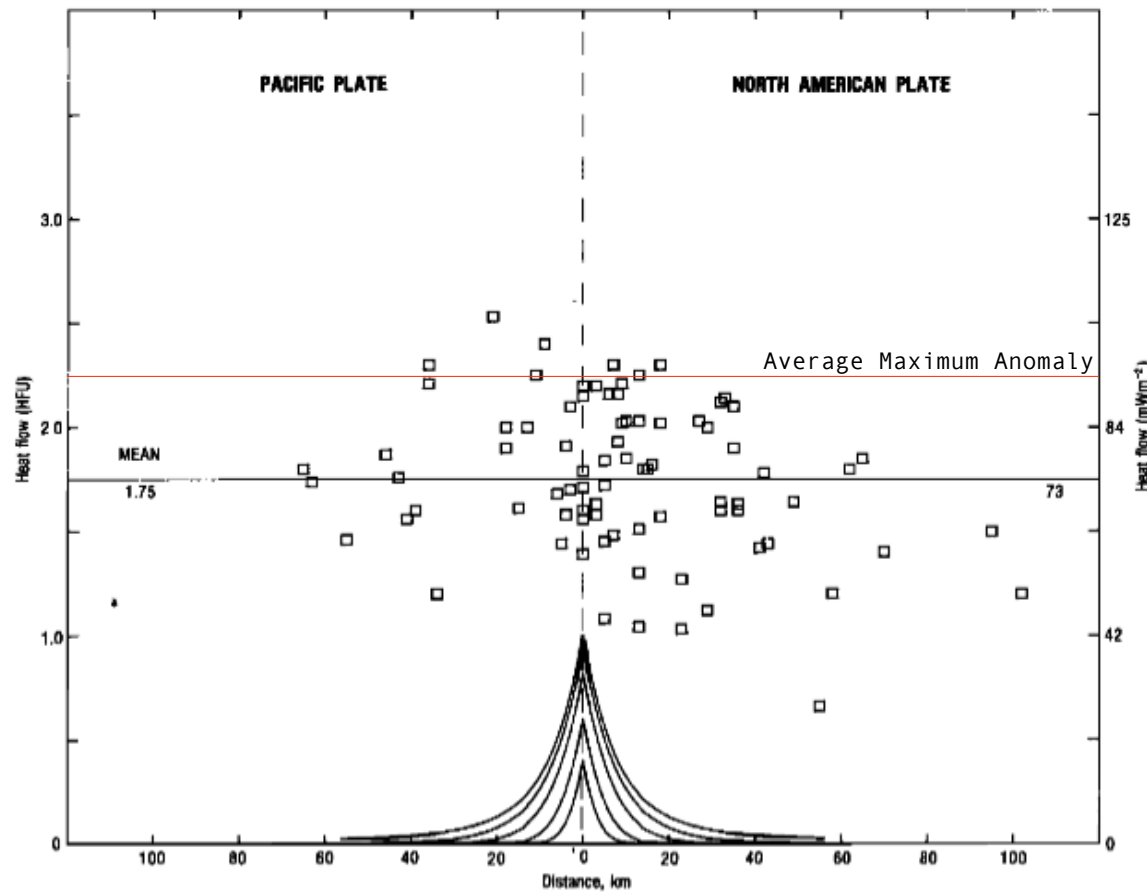
- Substitute $q(x,a)$ and $f(a)$ into our equation for $q(x)$ and get the following:

$$q(x) = \frac{2v\mu\rho_c g}{4\pi} \int_{a_1}^{a_2} \frac{a^2}{x^2 + a^2} da$$

- Finally, use the integral identity for an arc tangent function to get the final expected surface heat flow anomaly!

$$q(x) = \frac{2v\mu\rho_c g}{4\pi} \left[a - x \tan^{-1} \left(\frac{a}{x} \right) \right] \Big|_{a_1}^{a_2}$$

Observed Heat Flow Measurements

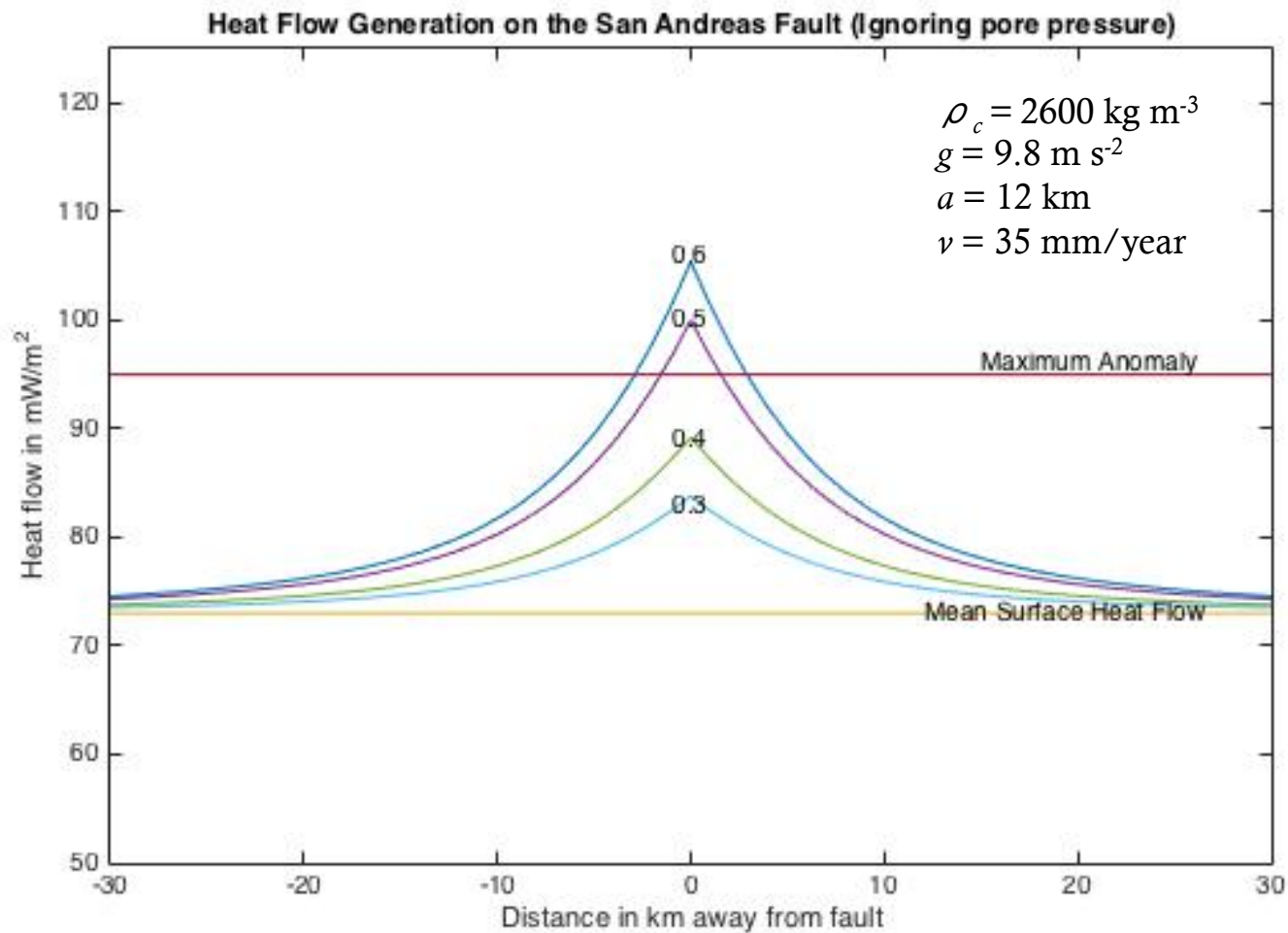


Observed heat flow
By Lachenbruch
& Sass (1980)

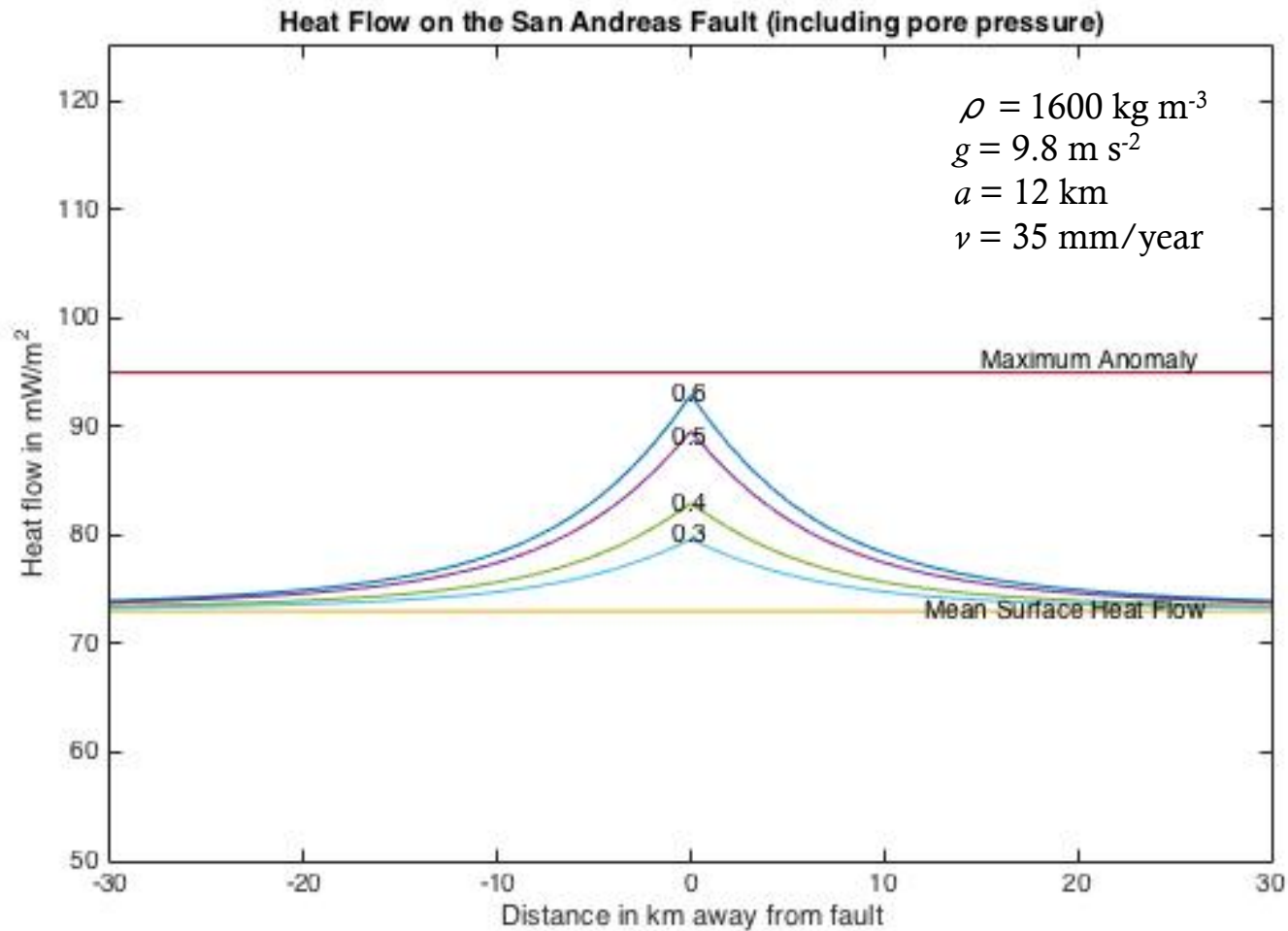
Mean Surface
Heat Flow
- 73 mW m⁻²

Average Maximum
Anomaly
- 94 mW m⁻²

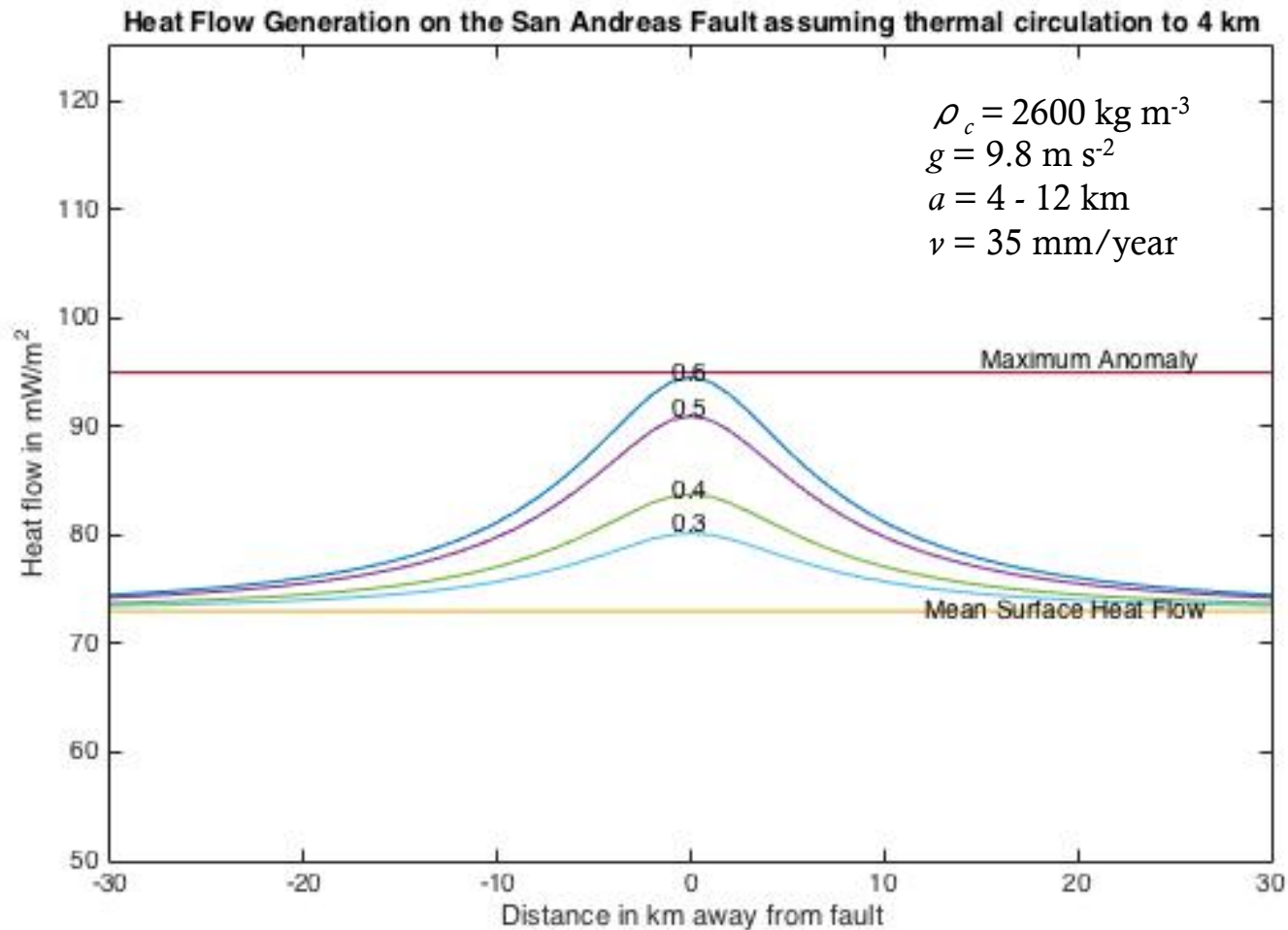
Expected Heat Flow Anomaly



Expected Heat Flow Anomaly (including pore fluid pressure)



Expected Heat Flow Anomaly (including hydrothermal circulation)



Discussion

- No evidence for significant hydrothermal circulation along the San Andreas (Lachenbruch & Sass 1980, Turcotte et al 1980)
- Error may be associated with coefficient of static friction
 - Evidence for talc found in serpentinite could account for low μ for creeping portions of SAF (Moore & Rymer, 2007)
- Still a large debate as to whether the San Andreas Fault is a strong or weak fault (Saffer et al 2003)

References

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