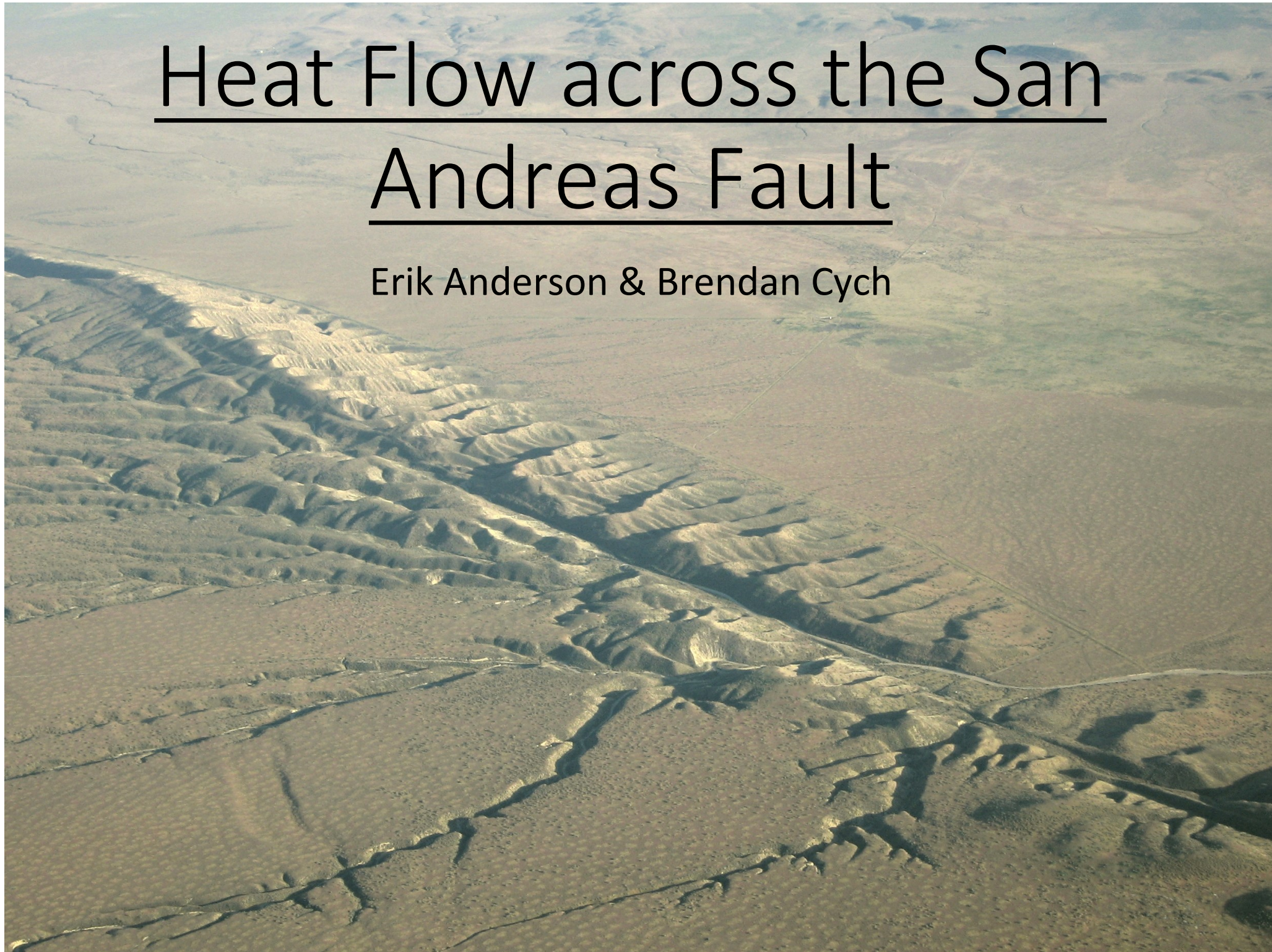


# Heat Flow across the San Andreas Fault

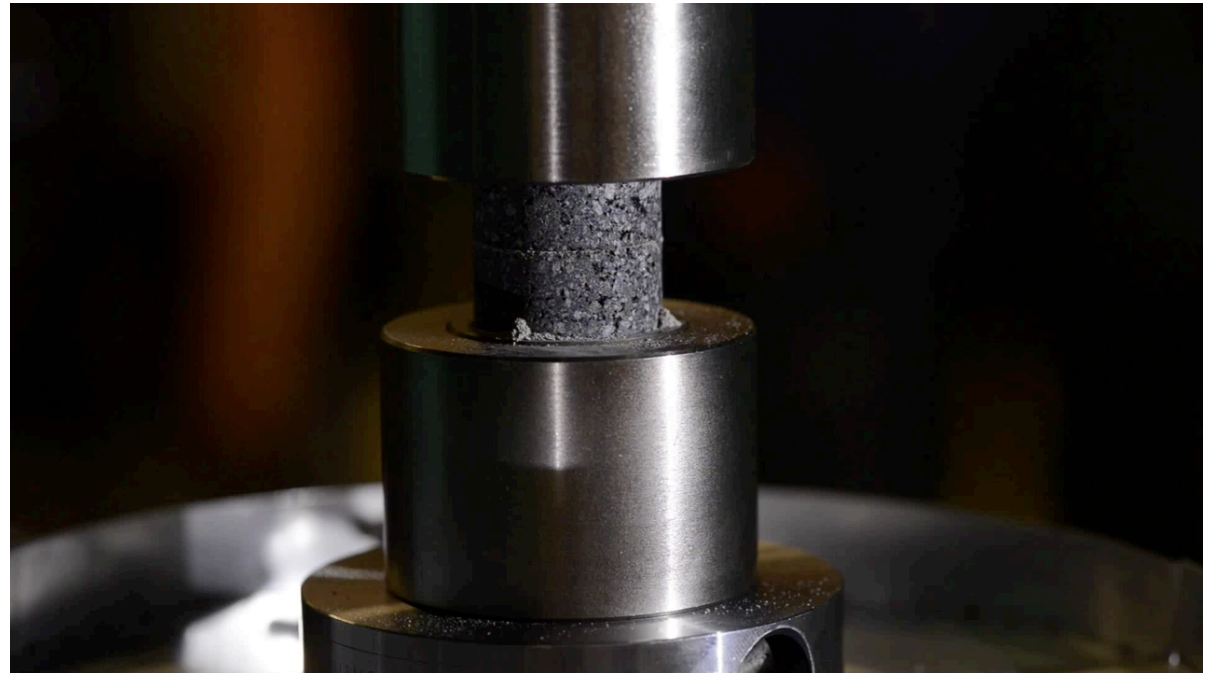
Erik Anderson & Brendan Cych



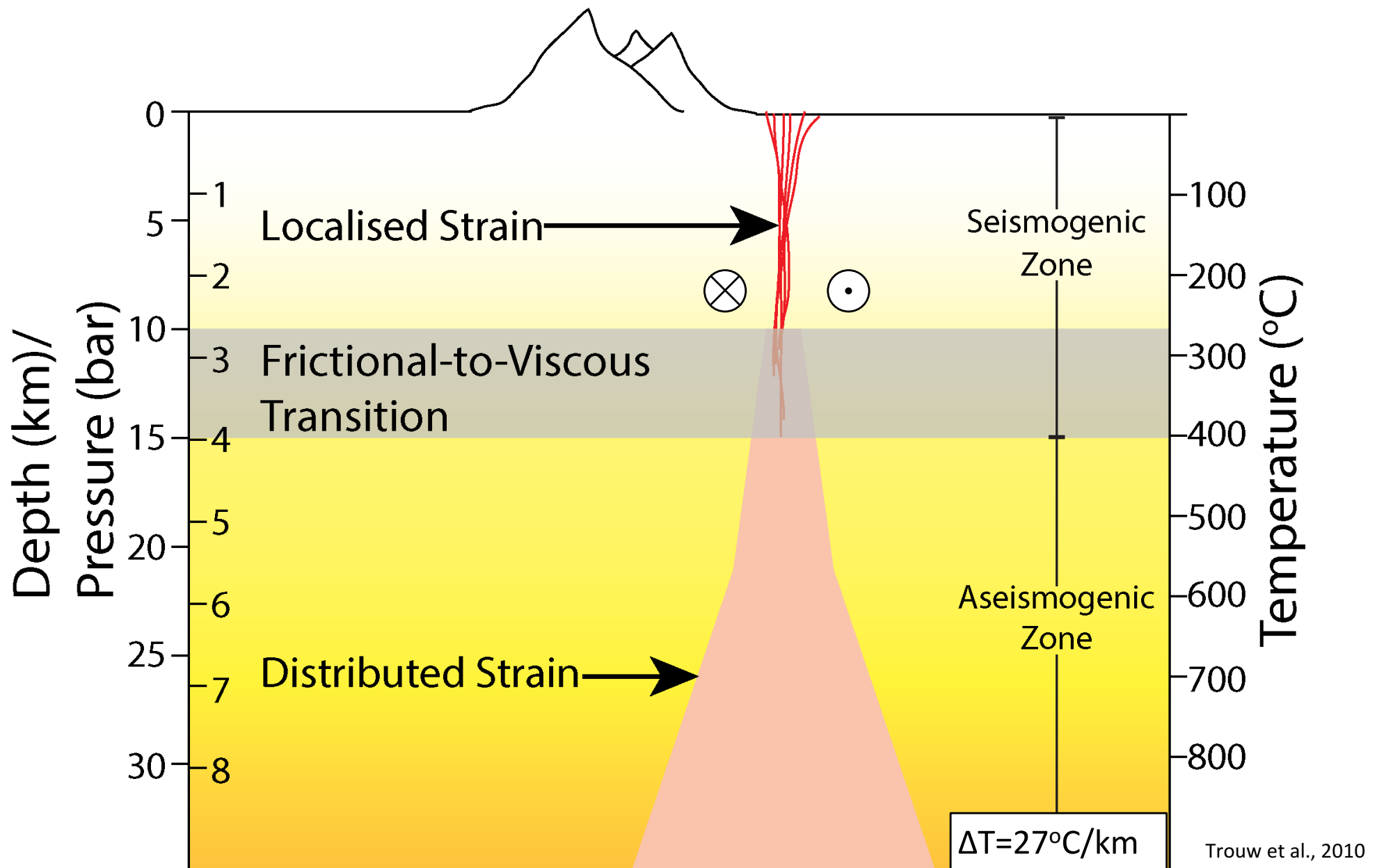


# Friction Along Faults Generates Heat

- Energy from slip partitioned into:
  - 1) Fracture creation
  - 2) Seismic radiation
  - 3) Thermal energy
- What component plays the largest role?

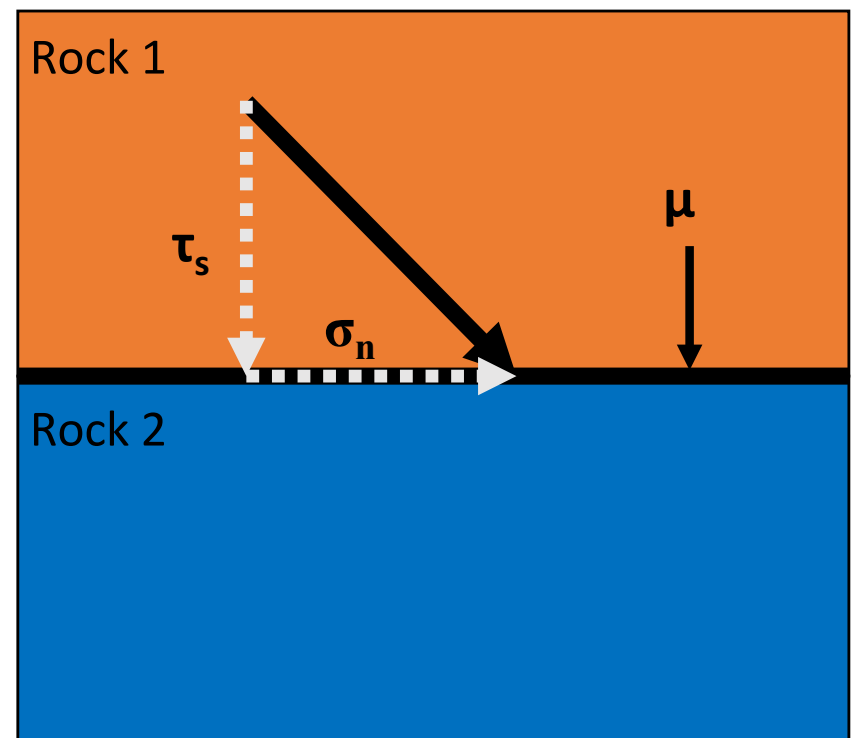


# Earthquakes Occur Along Faults in the Upper Crust



# Radiated Seismic Energy Measurements Underestimate Theory

- $\tau_s = \mu \rho_c z$ 
  - $\mu \sim 0.60$
  - $\rho_c - 2600 \text{ kg/m}^3$
  - $z$  – depth (m)
- Average stress drop determined by integrating across depth of seismogenic zone ( $\sim 12\text{km}$ )
- $\bar{\tau}_s = \frac{1}{D} \int_0^D \mu \rho_c g z$
- $\bar{\tau}_s = \frac{1}{2} \mu \rho_c g D = 92 \text{ MPa}$
- Seismicity observes stress drops of 0.1-10MPa



# Setting up the equation and boundary conditions

- Need to consider a line source at  $z=a$  to represent heating

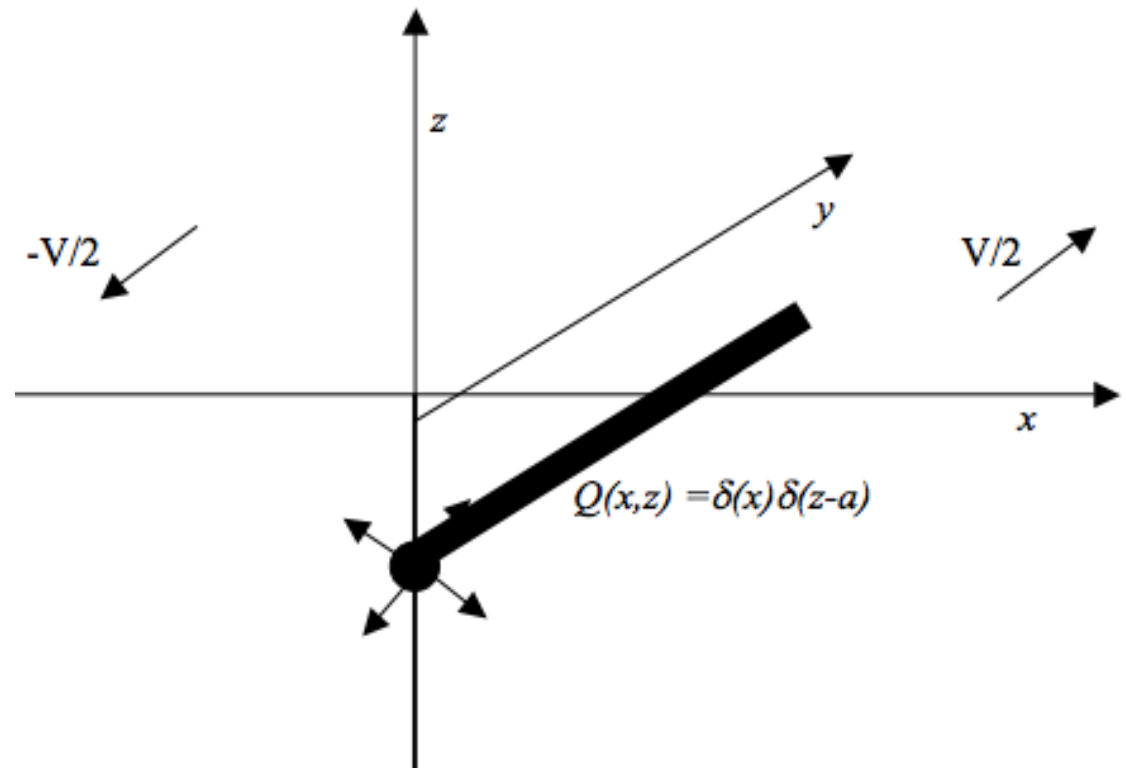
- Initial formula for heat flow given by

$$\nabla^2 T = \frac{1}{k} Q(x, z) = \frac{1}{k} \delta(x) \delta(z + a)$$

- Boundary conditions

$$T(x, 0) = 0 \quad \lim_{|z| \rightarrow \infty} T(x, z) = 0$$
$$\lim_{|x| \rightarrow \infty} T(x, z) = 0$$

- We will need a heat sink to satisfy these, placed at  $z=-a$



# Solving the differential equation for $dT/dz$

$$\nabla^2 T = \frac{1}{k} Q(x, z) = \frac{1}{k} \delta(x) \delta(z + a)$$

- We already solved our differential equation for heat flow in class. (Notes on Fourier transforms).
- Take the Fourier transform of both sides, using the derivative property on the LHS and definition of the delta function on RHS
- Take the inverse transform in the Z direction, using the Cauchy residue theorem to make this easier.
- Take the inverse transform in the x direction, using the derivative property with respect to z to get  $dT/dz$

## Solving the differential equation for $dT/dz$

- Note that our solution is different to in the notes, as we have a conduction term

$$\frac{\partial T(x, z)}{\partial Z} = -\frac{1}{2\pi k} \frac{z + a}{(x^2 + (z + a)^2)}$$

- We need to add the line sink to the equation so we obtain

$$\frac{\partial T(x, z)}{\partial Z} = -\frac{1}{2\pi k} \left\{ \frac{z + a}{(x^2 + (z + a)^2)} - \frac{z - a}{(x^2 + (z - a)^2)} \right\}$$

## Finding the surface heat conduction using Fourier's Law

- As we have included conduction in our equation, we can solve for the surface heat flow using Fourier's law of thermal conduction

$$q = -k \frac{dT}{dz}$$

$$q(x, z) = \frac{1}{2\pi} \left\{ \frac{z + a}{(x^2 + (z + a)^2)} - \frac{z - a}{(x^2 + (z - a)^2)} \right\}$$



## Obtaining the Green's Function

- For our surface heat flow, we solve for  $z=0$

$$q(x, 0) = \frac{1}{\pi} \left\{ \frac{a}{x^2 + a^2} \right\}$$

This gives us a Green's function which we can then convolve with an arbitrary source.

$$G = \frac{1}{\pi} \left\{ \frac{z}{x^2 + z^2} \right\}$$

# Convolution with the Green's Function

- Our heat source is not a line source at depth, it's a plane, where the heat flow at depth  $z$  is given by

$$q(z) = u\tau(z)$$

- We can then convolve this with our Green's Function to get our surface heat flow for this source.

$$q(x) = \frac{u}{\pi} \int_0^D \left\{ \frac{z \tau(z)}{x^2 + z^2} \right\} dz$$

## Convolving with the Green's Function

- We can use our initial formula for the normal stress, given by  $\tau(z) = \mu\rho_c g z$
- We can then plug this into our equation for the surface heat flow.

$$q(x) = \frac{\mu\rho_c g u}{\pi} \int_0^D \frac{z^2}{x^2 + z^2} dz$$

## Solving this integral

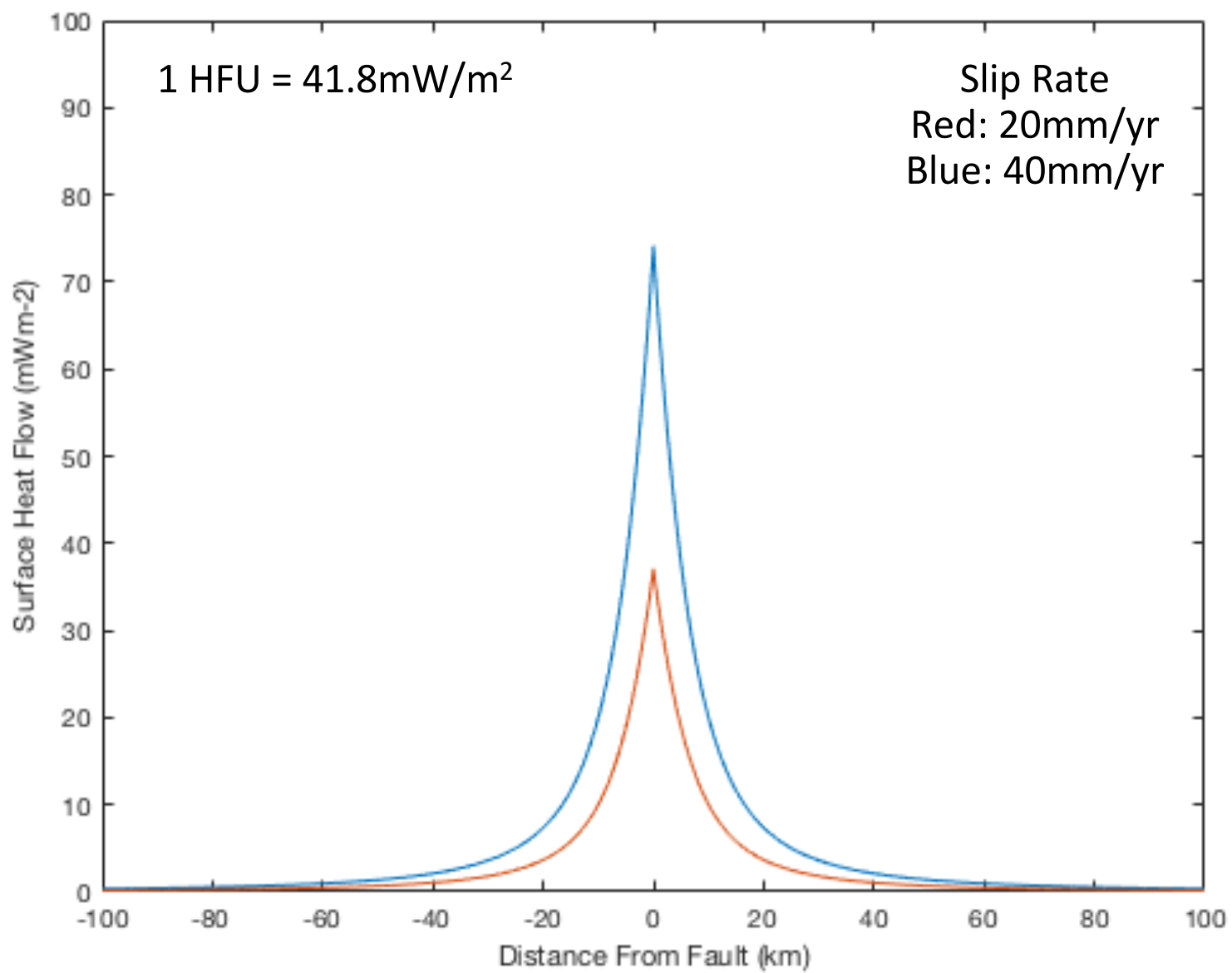
We can rearrange the equation in the integral

$$\frac{z^2}{x^2 + z^2} = \frac{z^2 + x^2 - x^2}{x^2 + z^2}$$

$$= 1 - \frac{x^2}{x^2 + z^2}$$

$$q(x) = \frac{\mu \rho_c g u}{\pi} \int_0^D 1 - \frac{x^2}{x^2 + z^2} dz$$

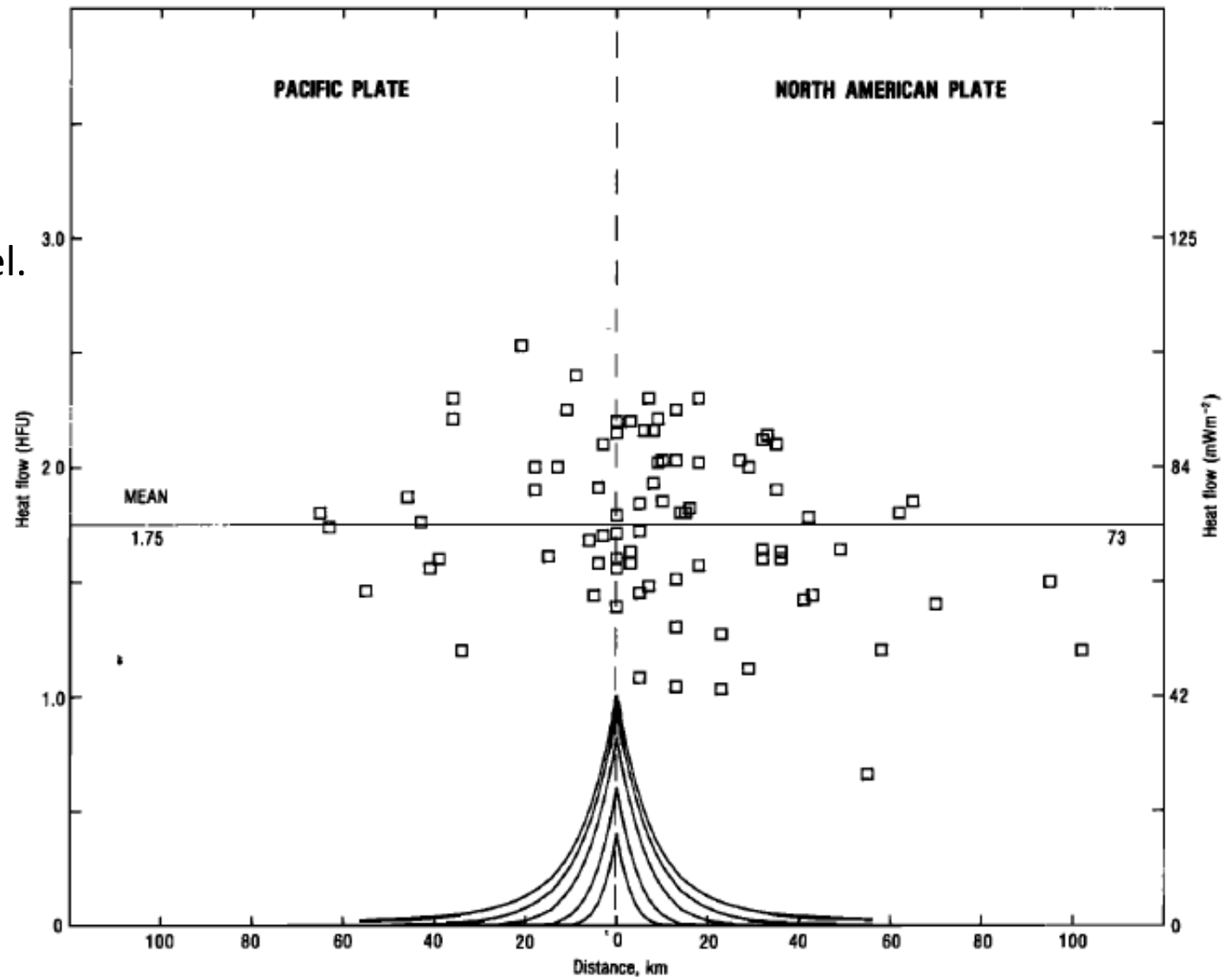
$$= \frac{\mu \rho_c g u}{\pi} \left\{ D - x \tan^{-1} \frac{D}{x} \right\}$$



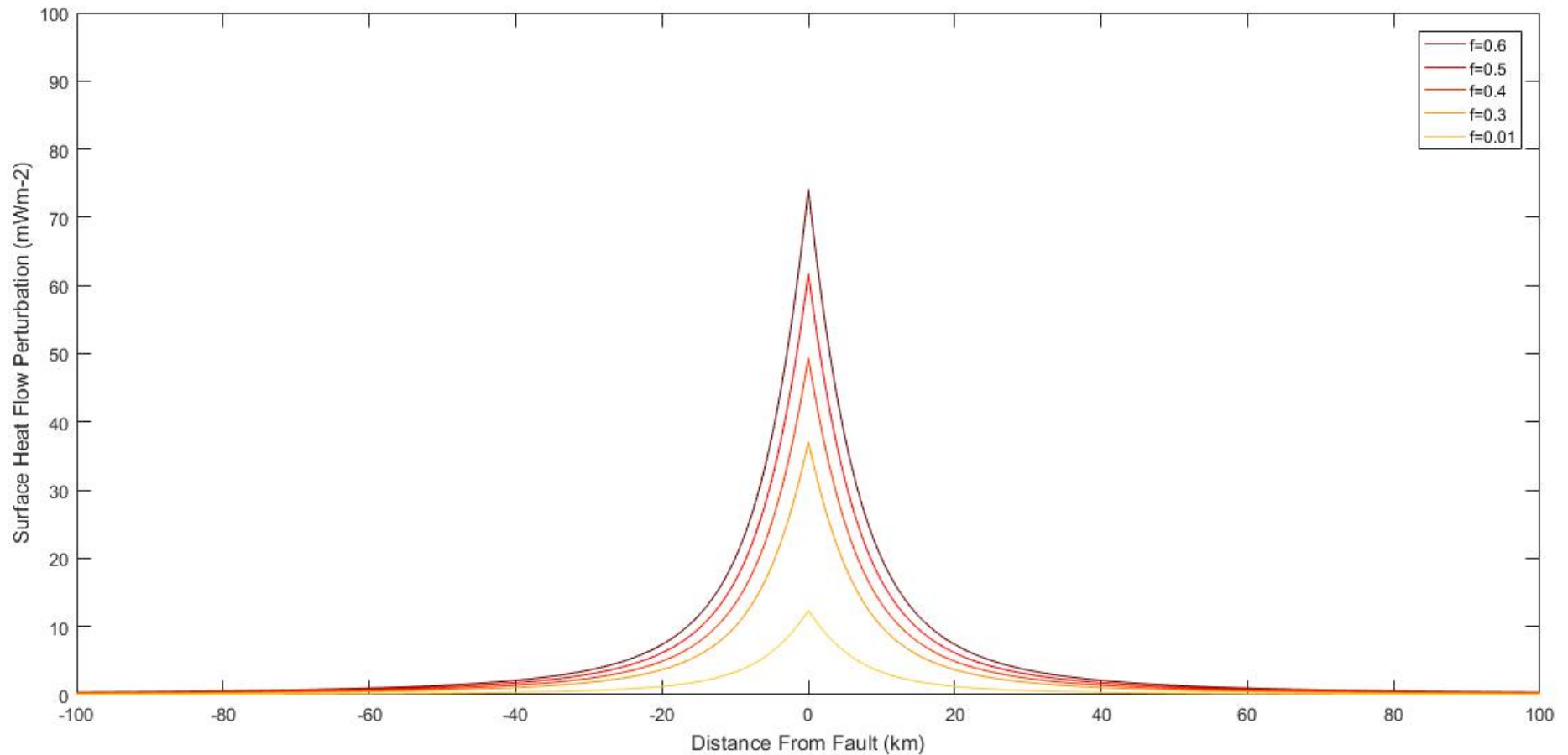


# Comparing Model with Surface Observations of Heat Flow

- Lachenbruch and Sass (1980) observe no perturbed surface heat flow measurements predicted by their model.



# Changing Frictional Coefficient Cannot Produce Heat Flow Anomaly



## Accounting for Hydrothermal Circulation

$$q(x) = \frac{\mu(\rho_c - \rho_w)gu}{\pi} \int_d^D 1 - \frac{x^2}{x^2 + z^2} dz$$
$$= \frac{\mu(\rho_c - \rho_w)gu}{\pi} \left\{ (D - d) + \left( x \tan^{-1} \frac{d}{x} - x \tan^{-1} \frac{D}{x} \right) \right\}$$

# Hydrothermal Circulation Broadens Heat Anomaly Profile

