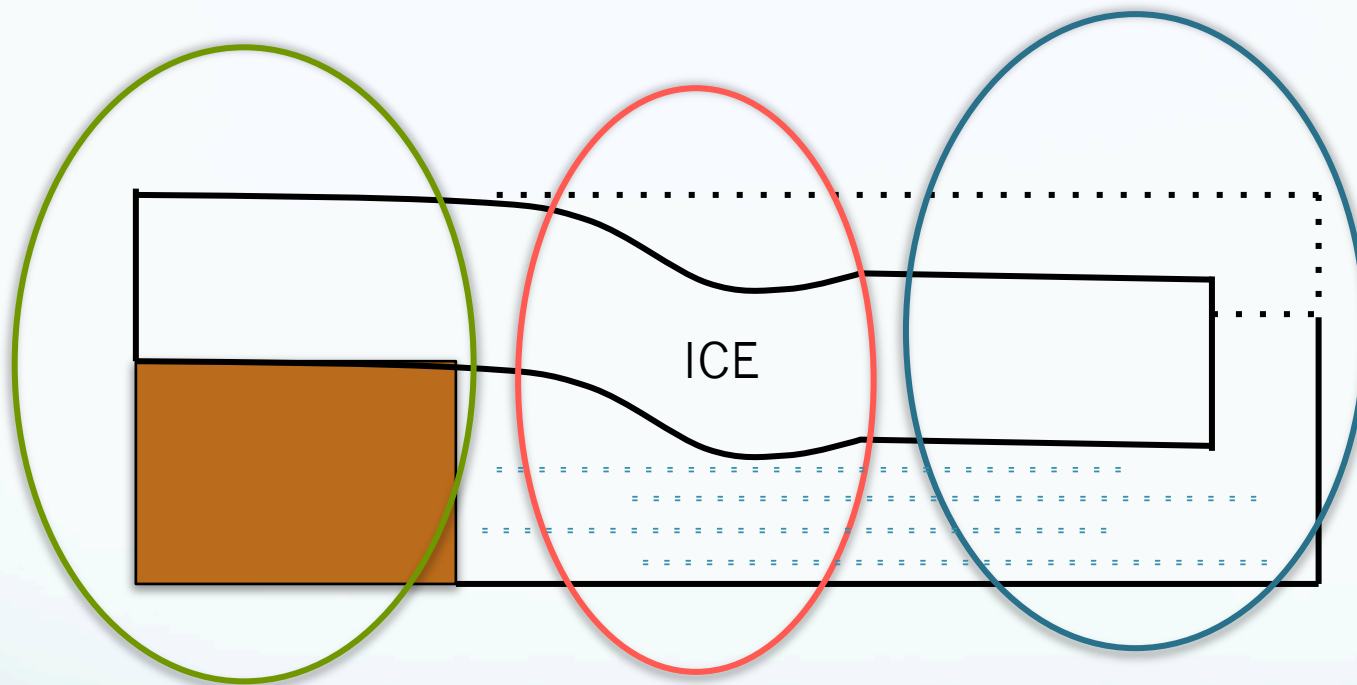


TIDAL FLEXURE OF ICE SHELF MARGIN

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HW6
Introduction to Geodynamics
2016

BUT WHY?

- *Power dissipation*
- *Glacier fabrics affecting flow*
- *Ice shelf evolution*
- *Change in flexure indicates global warming*



Supported by basement

Floating (in motion with tide)

Hydrostatic pressure + internal stresses

Kinematic GPS technique



Tidal displacement profile

PART 1

- Elastic beam theory
- Derivation of elastic modulus

30 km wide, 150 km long, 2000 km thick

PART 2

- Application of the model to other data to find the elastic modulus



After Vaughan, 1995

Tidal cycle



[Sinha, 1978]

Effective Elastic Modulus= Truly elastic + viscoelastic response

Depends on :

- Load time and Temperature

Differential equation for deformation of elastic beam:

$$D \frac{\partial^4 w}{\partial x^4} = \rho g [A_0(t) - w(x)]$$

$$D = \frac{Eh^3}{12(1 - \nu^2)} = \text{flexural rigidity}$$

h = thickness of ice shelf

ν = Poisson's ratio

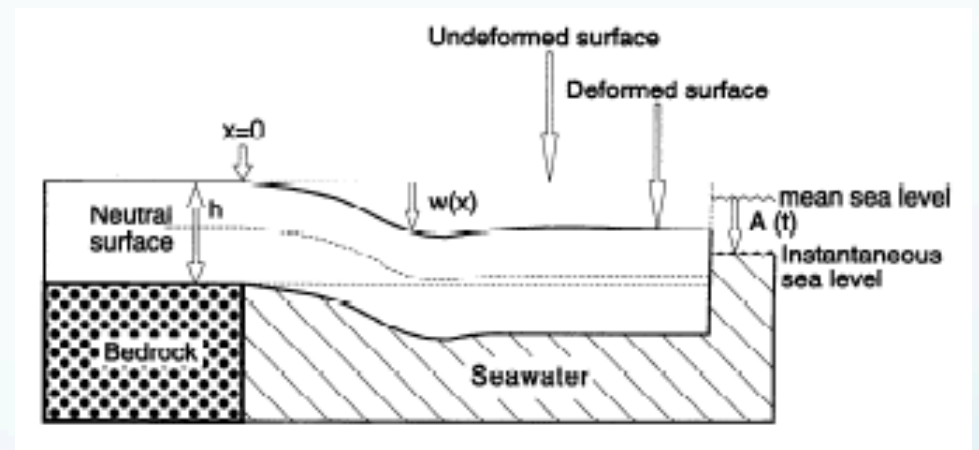
E = elastic modulus

ρ = density of sea water

g = acceleration due to gravity of earth

$w(x)$ = vertical displacement of ice sheet surface

$A_0(t)$ = tidal displacement beyond influence of hinge zone



After Vaughan, 1995

$$D \frac{\partial w^4}{\partial x^4} = \rho g [A_o(t) - w(x)]$$

$$\frac{D}{\rho g} \frac{\partial w^4}{\partial x^4} + w(x) = A_o(t) \quad \dots\dots\dots(i)$$

Boundary conditions:
 $w = 0, \frac{\partial w}{\partial x} = 0$ at $x = 0$
 $w = A_o(t)$ at $x = \infty$

Assuming:

$$\frac{D}{\rho g} \frac{\partial w^4}{\partial x^4} + w(x) = 0$$

&

$$w(x) = C e^{mx}$$

Equ. (i) becomes:

$$\frac{D}{\rho g} \frac{\partial C e^{mx}}{\partial x^4} + C e^{mx} = 0$$

$$m = \sqrt{i} \left(\frac{\rho g}{D} \right)^{1/4}$$

$$w(x) = C e^{\sqrt{i} \left(\frac{\rho g}{D} \right)^{1/4} x}$$

Now, let's assume: $w(x) = C_2 \dots\dots (a)$
 $C_2 = A_0(t)$ [from (i)]

Also, from previous assumption:

$$w(x) = C e^{\sqrt{i} \left(\frac{\rho g}{D}\right)^{1/4} x} \dots\dots\dots (b)$$

Boundary conditions:

$$w = 0, \frac{\partial w}{\partial x} = 0 \text{ at } x = 0$$

$$w = A_0(t) \text{ at } x = \infty$$

Using the boundary conditions we get $C = -A_0(t)$

Adding up (a) and (b):

$$w(x) = A_0(t) \left[1 - e^{\sqrt{i} \left(\frac{\rho g}{D}\right)^{1/4} x} \right]$$

$$w(x) = A_0(t) \left[1 - e^{(i+1) \left(\frac{\rho g}{D}\right)^{1/4} x} \right]$$

$$w(x) = A_0(t) \left[1 - e^{\beta x} \cdot e^{i\beta x} \right]$$

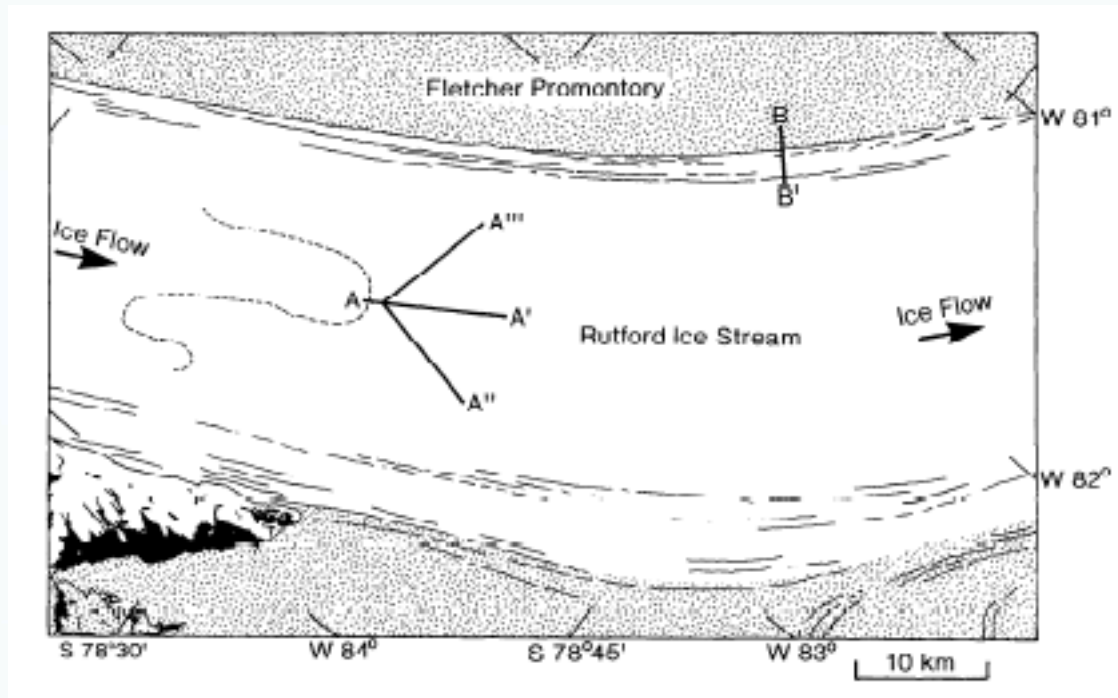
$$w(x) = A_0(t) \left[1 - e^{\beta x} (\cos \beta x + i \sin \beta x) \right]$$

$$\sqrt{i} = \frac{1}{\sqrt{2}} + \frac{i}{\sqrt{2}}$$

$$\beta = \left(\frac{\rho g}{4D}\right)^{1/4}$$

$$\beta^4 = 3\rho g \frac{1 - \nu^2}{Eh^3}$$

$$w(x) = A_0(t) \left[1 - e^{\beta x} (\cos \beta x + \sin \beta x) \right]$$

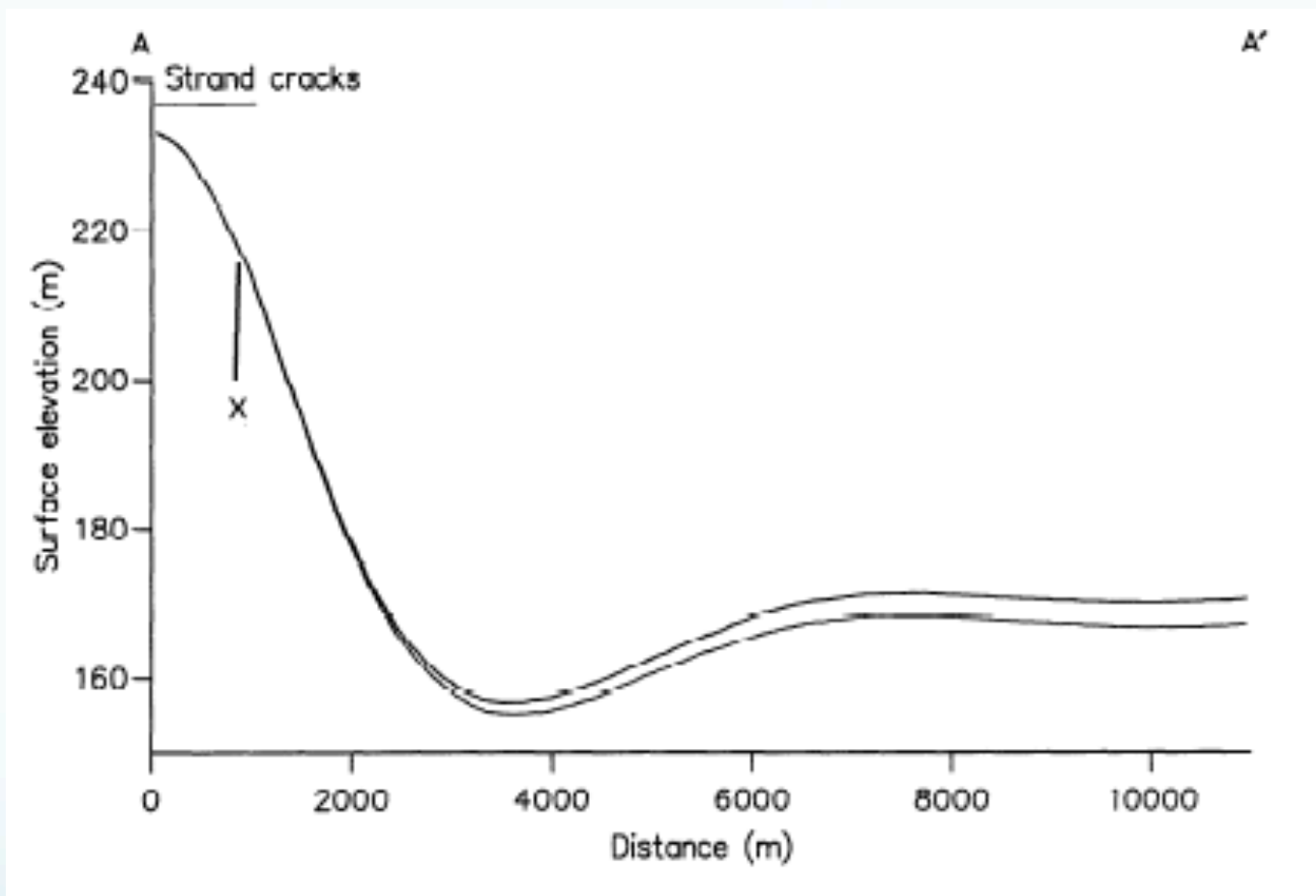


After Vaughan, 1995

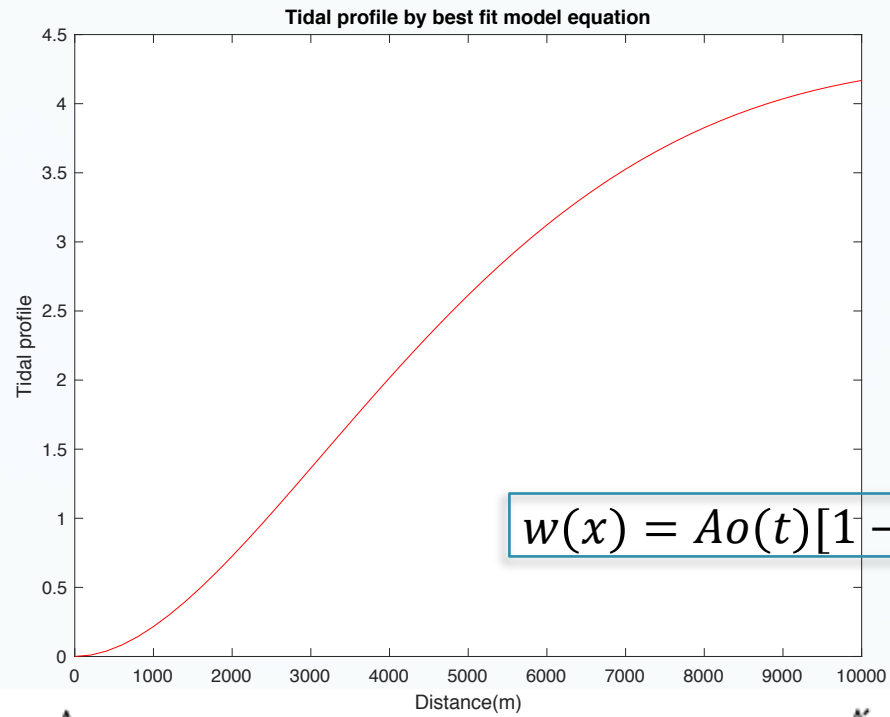
Tidal correction

$$d = \frac{e - e'}{p - p'} = \text{Tidal profile}$$

e, p = elevation, predicted tidal height at 1st visit
 e', p' = elevation, predicted tidal height at 2nd visit



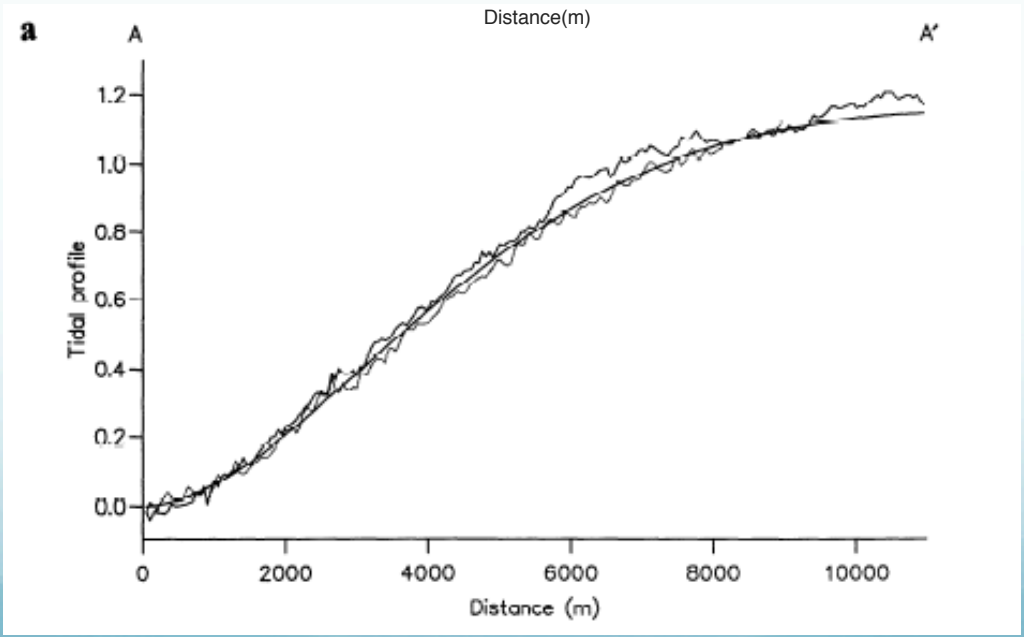
After Vaughan, 1995



$$A_0(t) = 4.1 \text{ m}$$

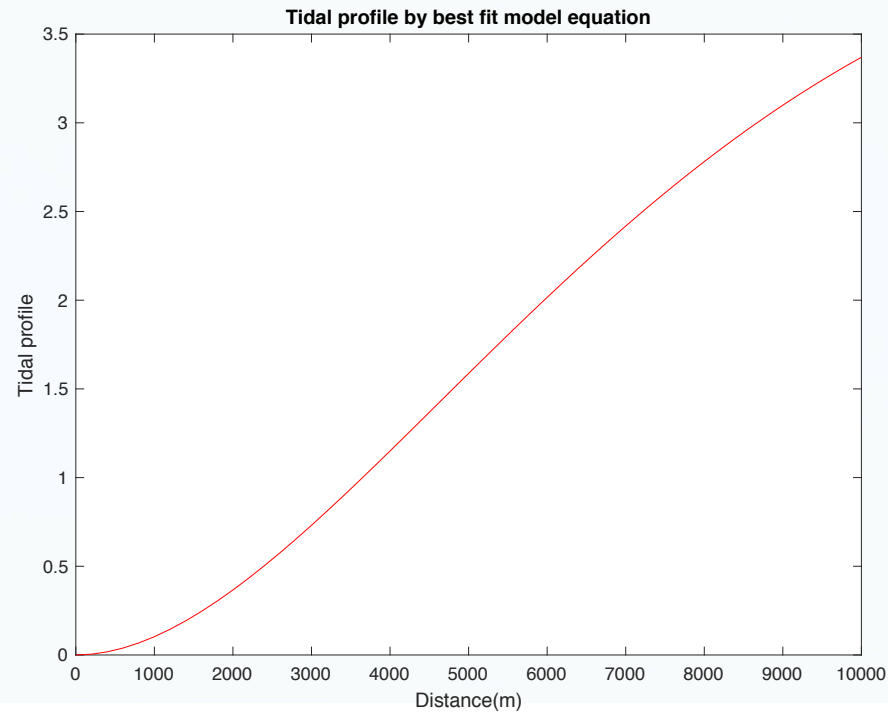
$$\beta = 2.5 \times 10^{-4}$$

$$w(x) = A_0(t) [1 - e^{\beta x} (\cos \beta x + \sin \beta x)]$$

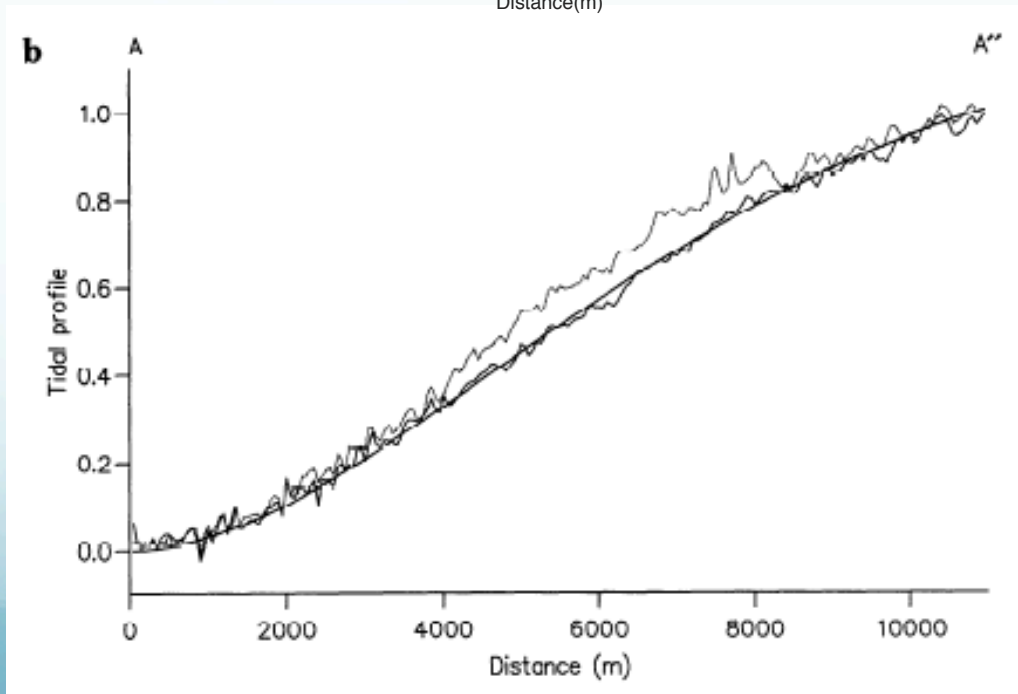


$$d = \frac{e - e'}{p - p'}$$

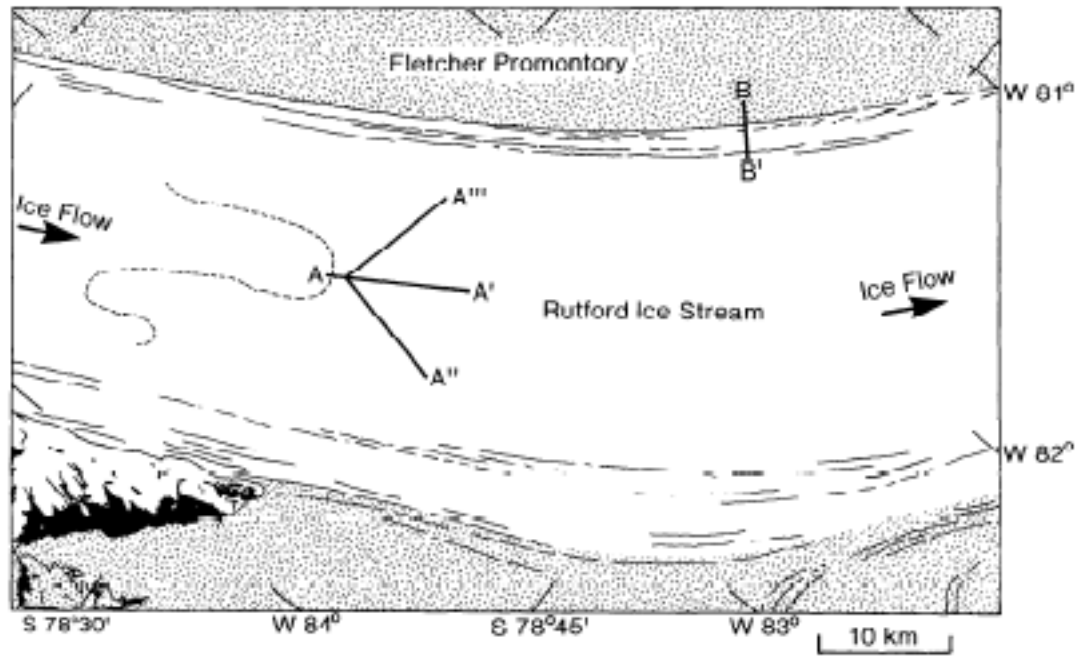
After Vaughan, 1995



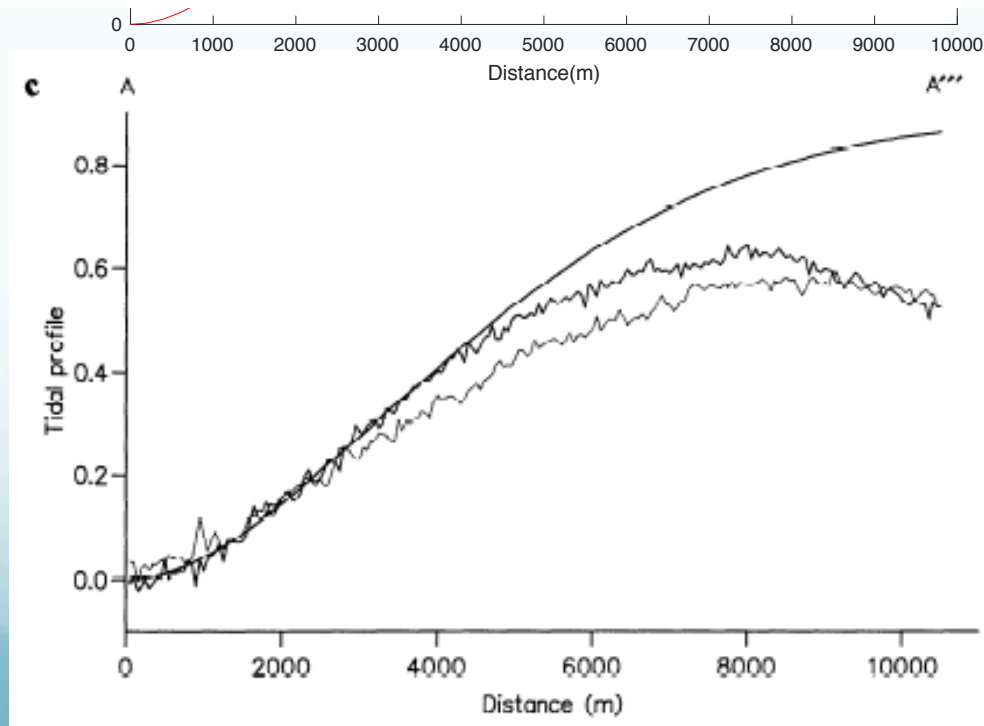
$$A_0(t) = 4.0 \text{ m}$$
$$\beta = 1.7 \times 10^{-4}$$



After Vaughan, 1995



$A_o(t) = 3.1 \text{ m}$
 $\beta = 2.5 \times 10^{-4}$



After Vaughan, 1995

$$\begin{aligned} A_o(t) &= (3.9 \pm 0.2) \text{ m} \\ \beta &= (2.43 \pm 0.43) * 10^{-4} \\ h &= 1550 \text{ m} \\ \nu &= 0.33 \end{aligned}$$

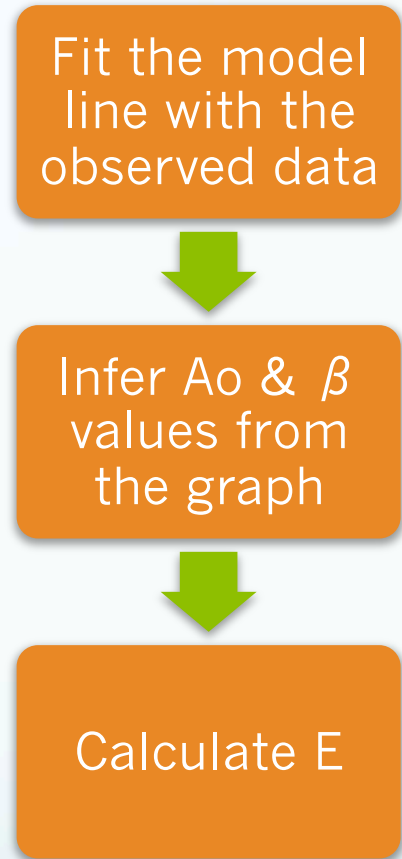


$$\beta^4 = 3\rho g \frac{1 - \nu^2}{Eh^3}$$

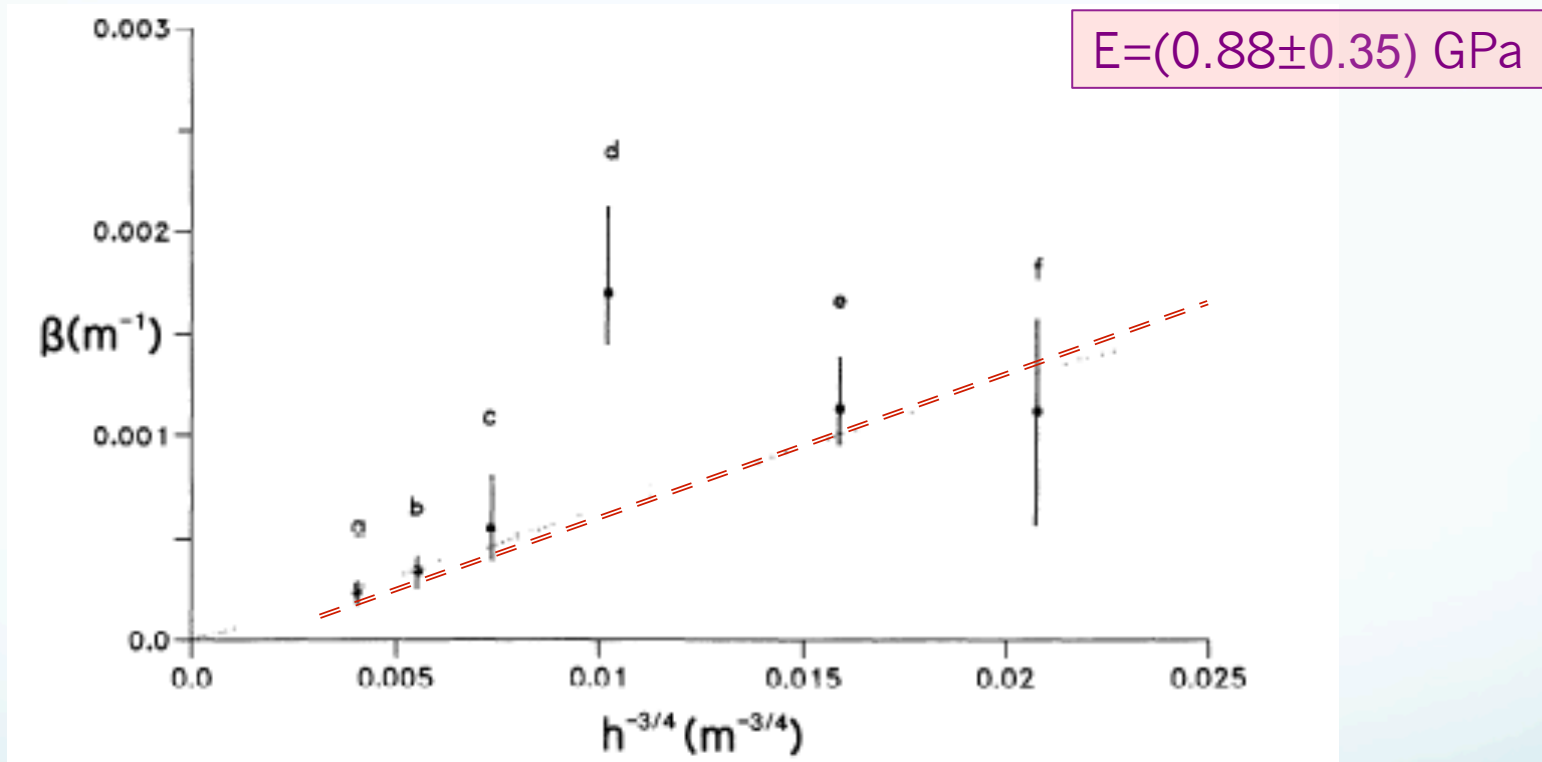


$$E = (0.57 - 2.4) \text{ GPa}$$

Location	Thickness (h) m
Doake Ice Rumples, Antarctica	1000
Bach Ice Shelf, Antarctica	250
Jakobshavns Glacier, Greenland	450
Ekstrom Ice Shelf, Antarctica	150-200
Maudheim Ice Shelf, Antarctica



$$\beta^4 = 3\rho g \frac{1 - \nu^2}{Eh^3}$$



After Vaughan, 1995

a= Rutford Ice Streaming Groundline
 c= Bach Ice Shelf
 e= Ekstorm Ice Shelf

b= Doake Ice Rumples
 d= Jakobshavns Glacier
 f= Maudheim Ice Shelf

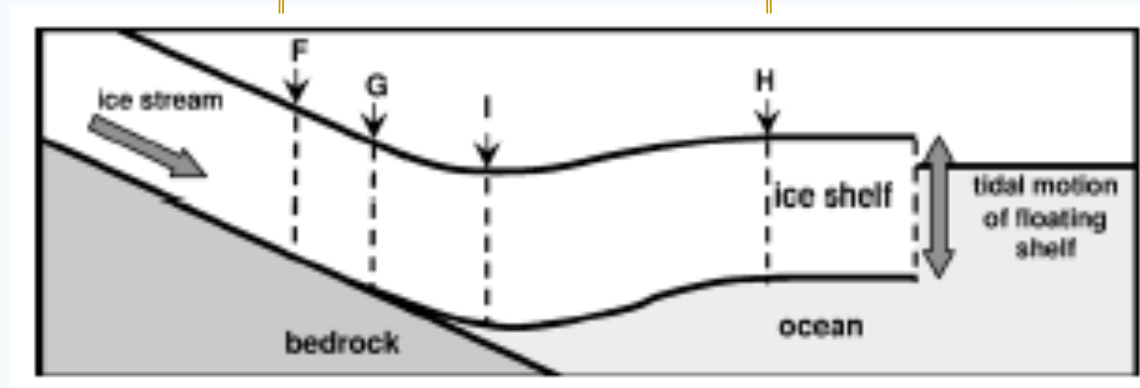
CONCLUSIONS:

- Average Elastic Modulus of 0.88 ± 0.35 GPa
- No evidence of variation of E with temperature
- No evidence of variation of E with structural style
- Tidal flexing can be considered in isolation from Ice Flow

LIMITATIONS:

- Not considered geometry of the bed rock
- Uniform tidal correction

Grounding zone



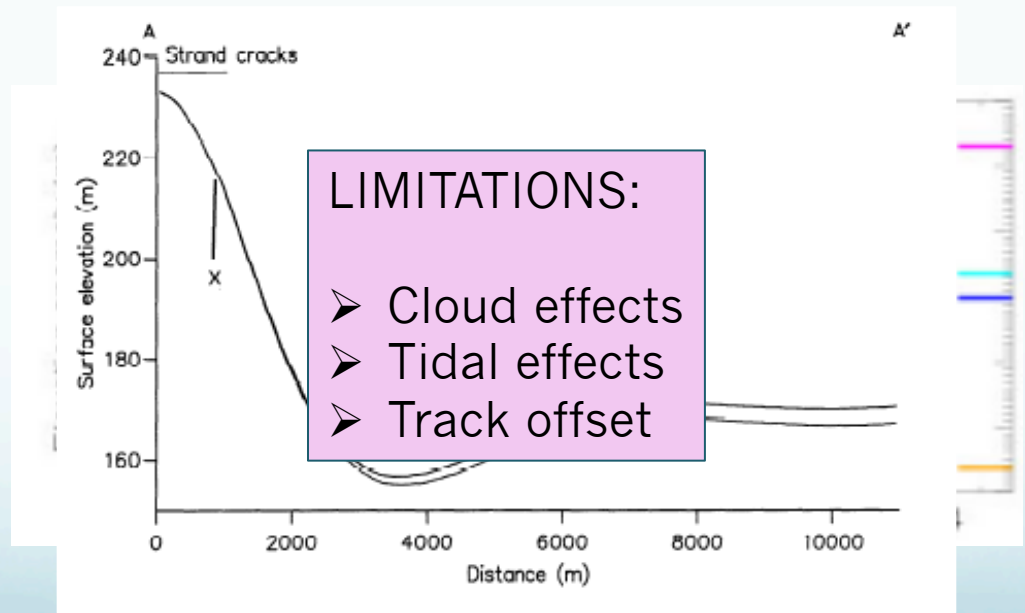
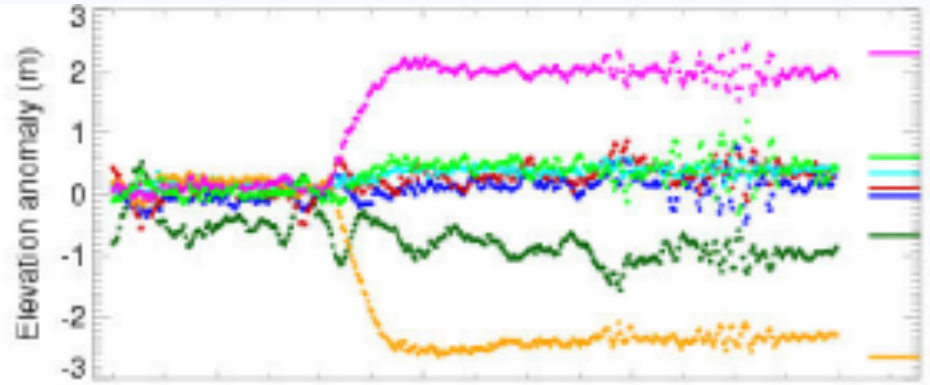
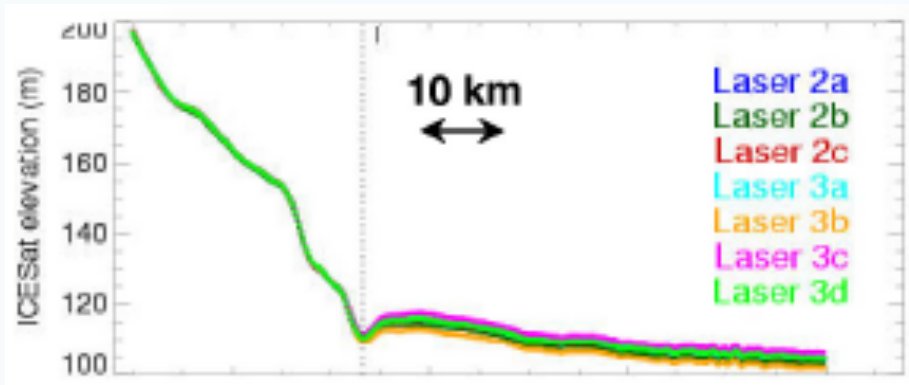
F=limit of ice flexure from tidal movement

G=limit of ice floatation

I=inflection point

H=seaward limit of ice flexure

[After Fricker and Padman, 2006]



After Vaughan, 1995

After Fricker and Padman, 2006

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- Vaughan D.G., *Tidal flexure at ice shelf margins*, Journal of Geophysical Research, Vol 100, Pages 6213-6224, 1994
- Fricker H.A. and Padman L, *Ice shelf grounding zone structure from ICESat laser altimetry*, Geophysical Research Letters, Vol 33, L15502, 2006
- Chuter S.J. and Bamber J.L., *Antarctic Ice shelf thickness from CryoSat-2 radar altimetry*, Geophysical Research Letters, Vol 42, Pages 10721-10729, 2015

THANK YOU

